ABT 2006 Spring Outage

Material Segment Wear Liners Fuel Injector diffuser/wear liner Ceramic Bricks Tips, 309SS 42" from PI Throat Segments # bags Super Abrade F3 burner 06-48595			107,100.00 92,000.00 7,050.00 4,570.00 798.00
	Sub Total	\$	211,518.00
Total Material			
Labor PO Release 320 PO Release 319 F3		\$ \$ \$	256,834.00 21,000.00 6,183.00
	Sub Total	\$	284,017.00
	Total	\$	495,535.00

2008		
ABT	Unit Price Quantity T	otal
Fuel Injectors price each		\$ 1,742,400.00
•	shipping 10%	\$ 174,240.00
15% discount if ordered by June 15, 2006	taxes	\$ 12,196.80
•	misc	\$ 20,000.00
	total materials + 10%	\$ 2,143,720.48
Labor	•	\$ 350,000.00
		\$ 2,493,720.48
	3% inflation	\$ 2,568,532.09
2008	,	
Power Industrial (PI)		
,	Unit Price Quantity T	otal -
Coal Nozzles		\$ 348,000.00
Conical Diffuser	· ·	\$ 58,800.00
Coal Deflector	T	\$ 17,280.00
Seal Plate		\$ 12,000.00
	Ŧ	\$ 20,000.00
		\$ 456,080.00
		\$ 547,296.00
	3	\$ 54,729.60
		\$ 3,831.07
		\$ 605,856.67
Labor	Total labor	\$ 350,000.00

Total	\$	955,856.67
I Utal	Ψ	000,000.07

On		

. , ,	Unit Price	Quantity	Tota	al
Coal Tip	\$ 4,110.00	48	\$	197,280.00
•	material change	20%	\$	236,736.00
	misc		\$	20,000.00
	shipping		\$	19,728.00
	taxes		\$	1,380.96
	Total materials		\$	277,844.96
	Total Labor		\$	350,000.00
	Total		s	627 844 96

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			Washington S			Order No06-6	
		PO	Box 211 Dono	ora, PA 15033	Proj∈	ect No. IGS	<u> </u>
Qty	Unit	Noun	Description Adjective	n Catalog #	Seller or Manufacturer	Unit Cost	Extension
24	ea	Air Flo	w Divider Cy.	linder, 33-3/4"	OD x 33" ID	\$2,385.00	\$57,240.00
		x 28" 1	ong, with one	e beveled end,	fabricated from		
		253MA.					
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				TOTAL	ESTIMATED COST		\$57,240.00
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Dent	Mgr/Sup			Station Manager	Date	Operating Agent	Date
L	2-/ Dab	· •	בי בי בי	cacton Manager	Date	Oberacing washing	. Date

TIATE	MINIOO	INTAIN FOWER SERVICE CORPORATION	Date: 12-Sep-07		
□ REQ	QUISITI	ON FOR CAPITAL EQUIPMENT	Req./PA No: 234	4385	
☑ PURCHASE AUTHORIZATION FOR EXPENSE ITEMS			P.O. No: Vendor:		
		e analysis and determine the failure mechanism on a ABT	FOB:	White the second	
Burner 7	1 1p		Ship Via:		
			Conf. To:		
Suggest	ed Ven	dor: <u>Thielsch Engineering</u> Accoun	t No00-2	SGX-402	
		195 Frances Ave. Work O	rder No. 06-0	3474	
		Cranston, RI 02910 Project	t No. IGSO	7-02	
Qty	Unit	Description Seller or Noun Adjective Catalog # Manufacturer	Unit Cost	Extension	
1	ea	Failure Analysis on ABT burner tip	\$15,000.00	\$15,000.00	
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INTERMOUNTAIN POWER SERVICE CORPORATION			Date: 27-Nov-07		
⊠ RE	EQUISIT	ION FOR CAPITAL EQUIPMENT	Req./PA No: 234	Req./PA No: 234410	
	D CITT I C		P.O. No:	P.O. No:	
□ PU	RCHAS	E AUTHORIZATION FOR EXPENSE ITEMS	Vendor:		
Purpos	e of Mate	erials, Supplies or Services:	Terms:	Sharina an a	
		xisting Unit 2 burner elbows and burner injectors and	FOB:		
	<u>lanned or</u>	ew injectors and elbows supplied by Siemens during Spring utage.	Ship Via:		
			Conf. To:	<u> </u>	
Sugges	sted Ven	1230 West 2600 South Work	unt No. 00-2 Order No. 06-0 ect No. IGSO	3474	
Qty	Unit	Description Seller or Noun Adjective Catalog # Manufacturer	Unit Cost	Extension	
48	ea	Replace existing burner elbow and burner injector	\$5,208.33	\$250,000.00	
		with new injector and elbow supplied by Siemens.			
	P. C.,	Same conditions as under site services contract			
	-	with AP&F #45603.			
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	N Vancoura de la constituto de la consti				
200140001400140014					
		TOTAL ESTIMATED COST		\$250,000.00	
<u>Siemer</u>	s per 0	allation of the new burner injectors and burner elboatober 31, 2007 meeting. 1-397-2763, Fax 801-397-1899, email www.apfpower.com	······································		
	ery requ	ested by [Date] <u>03-01-08</u> Originator <u>Ga</u>		Date	
-		-			

CAPITAL PROJECT JUSTIFICATION 2007-2008

JOB.NO:

IGS07-B

W.O. # 06-03474-0

TITLE:

Unit 2 burner injector / burner replacement

DESCRIPTION:

Repair or replace all 48 ABT burner nozzles during the 2008, Unit 2 outage.

JUSTIFICATION:

OBSOLESCENCE

WHAT IS OBSOLETE:

ABT burner injector

WHY OBSOLETE:

Damaged during operation

WHEN OBSOLETE:

Needed for 2008 Planned Outage

WHY IS IT STILL NEEDED:

ABT burner deficiencies

ADDITIONAL DETAIL:

Severe damage found during 2006 planned outage. Repaired/patched as best as possible

with time allowed.

COST ESTIMATE:

07-08

Engineering Labor \$ 2,000 Installation Labor \$ 360,500 Contractor Labor \$ 0

Material

\$2,214,500

Job Total

\$2,577,000

ALTERNATIVES:

none

EFFECT OF DEFERRAL:

Damaged burners may result in loss of generation and possibly an extended forced outage.. Existing ABT burners only made it two years due to an apparent design problem with the

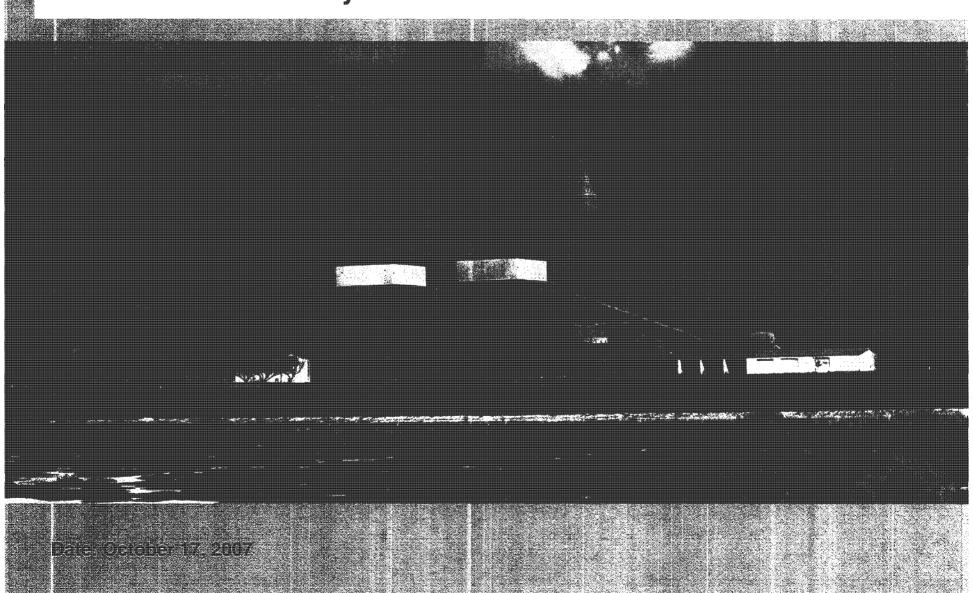
original purchased burners.

CAPITAL PROJECT JUSTIFICATION 2007-2008

<u>PROJECT HISTORY:</u> ABT burners were purchased and installed Spring 2004 on Unit 2. Damage to burners were found during an inspection on F row following a burner line fire October 2005. Burners continued to show increased erosion problems. Coal tip segment wear liners and a diffuser/wear liner for the injector were purchased and installed during the 2006 planned outage due to time and money constraints.. Severe cracking of the injector tip was also found on many burners during the planned outage. 15 of the worst tips were removed and replaced with another design.

Intermountain Power Service Corp. ABT Siemens Warranty Claim

SIEMENS



Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

MABIL was awarded a contract in 2003 for the material supply of low NOx burners replacing Texts that B&W burners that had operated since 1992.

The base contract was for material supply only of 48 low NOx burners, 48 ABB Scanners plus air flow measuring equipment.

Approximately one year after commercial operation, the unit suffered a fire in one burner that the try of the fuel injector. During the following Spring outage. Inspection revealed additional negries had oracles and excessive framing of the fuel piping and nozzles.

Abril 2007, Stemens BTS and IPSC minated a Six Sigma investigation to determine the root cause of the or the problems with the burners.

Siemens ETS and IPSC agreed on an issue statement with the five items:

- (1) The alloy nozzle tip is cracking
- 2) There is material loss at the following locations:
 - The Burner nozzle tio
 - The "X" vane at the coal pipe elbow
 - The dourner barrel
- The burner barrehis experiencing permanent deformation
- Establish the correct primary airflow for normal operation
- 5.) Definition of requirements for cooling air when the burner is out of service

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

The Sir Signia Hoot Cause analysis followed the five steps for a Six Sigma Project

Define: clear definition of the problem and the aim of the project.

During the define stage, all available correspondence was collected; contract documents were collected, the number parties were interviewed and an issue Statement developed and agreed to

Weastife: Examination of the current process and collection relevant data for future analysis

The AFT design records were reviewed, the existing pulverizer performance at IPSC was documented and metallungical analysis of the cracked burner nozzle was performed.

Analyze: Evaluation of the measured results and identification of the actual cause of the problem

CED analysis and thermal modeling of the nozzles using the operating parameters as measured during the bullerizer testing was performed. A root cause analysis was generated:

Into FeMe: 4Selection and implementation of the solution

A new him per design was generated using the information collected during the Define and Measure stage and CED analysis undertaken to verify changes will

Control of the changed process

The differences between the original design and the revised design need to be implemented and documented

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

Executive Summary

- he allow now letter tip cracking is the result of erosion of the wall thickness in the nozzle due to higher than

 our right arrang coal flow. The thinner wall section weakened the nozzle to the point that the nozzle

 could not accommodate the stress generated by the differential expansion between the stainless steel

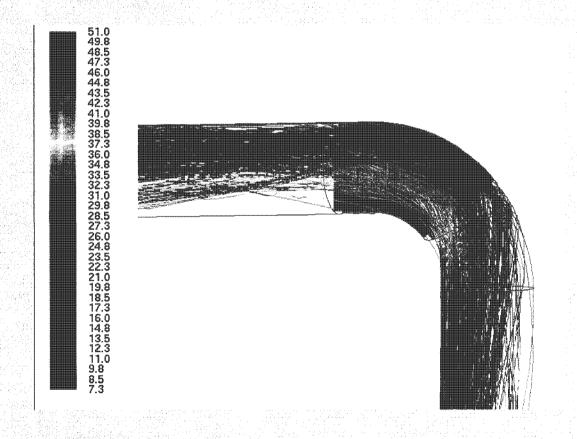
 tozzle and the carbon steel barrel.
- pere is material loss at the burner nozzle tip. "X" vane at the coal pipe elbow and the burner barrel are a less that coal and air flows being higher than design plus stratification of the coal particles in the coal burner barrel are a less that the coal particles in the coal burner barrel are a less that the coal burner barrel are a less that the coal particles in the coal burner barrel are a less that the coal burner barrel are a less that the coal particles in the coal burner barrel are a less that the coal particles in the coal burner barrel are a less that the coal particles in the coal burner barrel are a less that the coal particles in the coal burner barrel are a less that the coal burner barrel are a l
- The buliner bairiel is experiencing permanent deformation due to higher than expected temperatures at the inferior barrel and barrel. The burner barrel will use a SS spool piece to extend back into the burner barrel.
 - The plant has not been operating per the B&W with philipping and been operating per the B&W with philipping are curve supplied in the contract did not reflect the levision by B&W in 1992. Also, the plant has been operating at higher seal air flows in the plant has been operating at higher seal air flows.

 If the plant is out of service—the Operations and Walnier are wall have to be revised to address out of service operation.

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

Erosion and Mill Air Flow



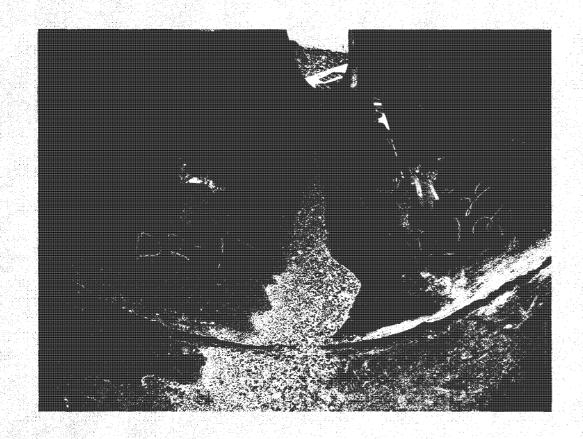
The CFD model shows the coal particles are stratified entering the elbow. The original kicker assembly with the X-vane that was modified to retain the clean out port will not last in the high velocity stream of concentrated coal particles with the higher coal flow.

The revised fuel injector design will increase the cross sectional area of the nozzle to reduce velocities, lengthen and flatten the slope of the transition ramp and replace the round elbow with a "Flat back" design to allow dispersion of the coal particles across the flow area of the nozzle.

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

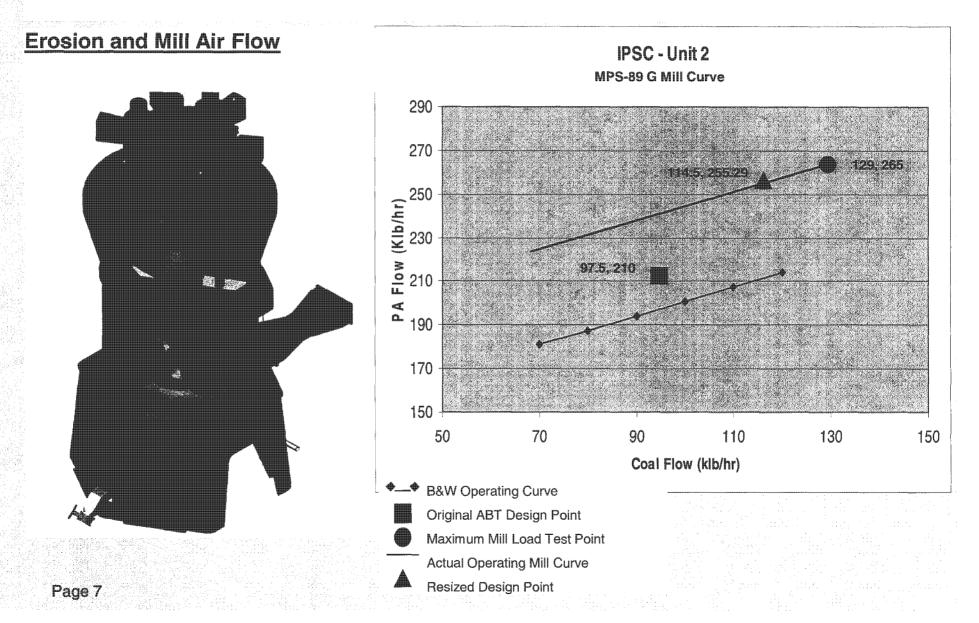
Erosion and Mill Air Flow



Erosion is originating at the transition slope from the round barrel to the 6 lobe exit. This is consistent with the results of the CFD model. The metallurgical analysis performed by Tordonato Energy Consultants identified erosion as a the contributor cause of the nozzle cracking. The high temperatures at the weld between the nozzle and burner barrel increased the stress which also contributed to the cracking. There was no evidence of corrosion.

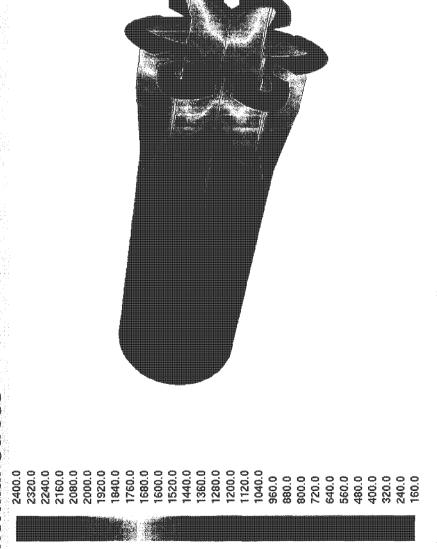
Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS



Intermountain Power Service Corp **ABT Siemens Warranty Claim**

Thermal Stress



stainless steel to make

the transition from the

nozzle to the barrel.

spool piece of 253MA

expected. The revised

fuel injector will use a

to the burner barrel to

be higher than

model shows that the The furnace radiation

heat conducted back

Sep 26, 2007 FLUENT 6.3 (3d, pbns, pdf20, rke)

minimize erosion. This

refractory tile to shield

injector shall use The revised fuel

he burner barrel from

adiation from the

furnace and to

of the secondary air on

not model the cooling

thermal model does

Contours of Static Temperature (f)

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

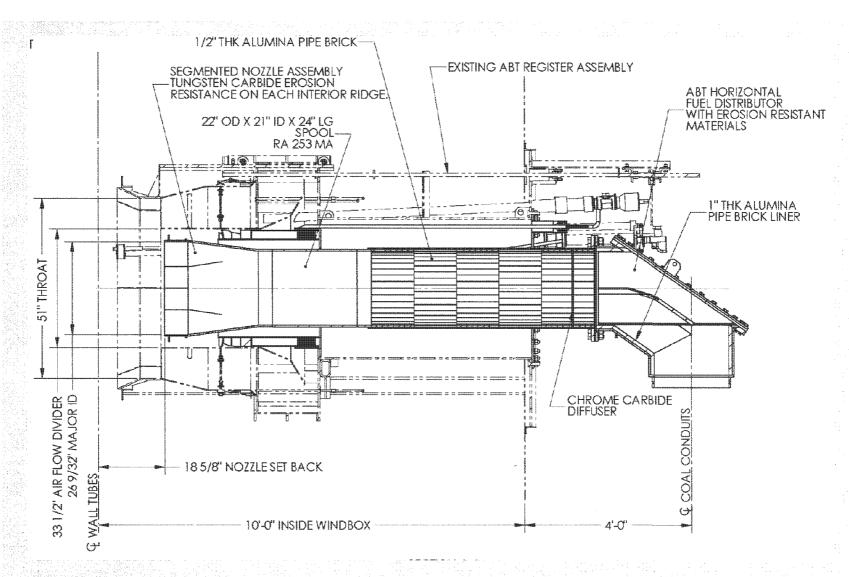
Thermal Stress



The off line burners are plugging with slag indicating that furnace gases are back flowing into the nozzle area. This creates very high temperatures that the nozzles were not designed for. A minimum air flow required to prevent this must maintained.

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS



Page 10

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

Next Steps

Close Out Six Sigma Program

•Commercial agreement between IPSC and Siemens Power Generation Inc

Agreement on Division of Responsibilities

INTE	ERMOU	INTAIN POWER SERVICE CORPORATION	Date: 27-Nov-07	Tanananan an a
⊠ RI	EQUISITI	ION FOR CAPITAL EQUIPMENT	Req./PA No: 234	1399
	_		P.O. No:	
□ P(JRCHASI	E AUTHORIZATION FOR EXPENSE ITEMS	Vendor:	
Purpos	se of Mate	erials, Supplies or Services:	Terms:	
		l injectors, x-vanes, and flat back elbows for Unit 2 burner	FOB:	WWW.obidoobidoobid.Millimm\uoobidoobidoA.Phy/millimmin
outage	repairs S	pring 2008.	Ship Via:	essignacessacessacessacessacessacessacessaces
			Conf. To:	1944 <u>/(1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (1944) (19</u>
Sugge	sted Ven	440 Alafaya Trail MC Q1-101 Work	unt No. 00-2 Order No. 06-0	03474
Qty	Unit	Description Seller or Noun Adjective Catalog # Manufacturer	Unit Cost	Extension
48	ea	Fuel Injectors	\$12,864.58	\$617,500.00
48	ea	x-vane	\$1,354.17	\$65,000.00 \$195,000.00
	-	TOTAL ESTIMATED COST		
		Allen, John Gallagher) and IPSC (George Cross, Denn at IPSC.	is Killian, Jerry	/ Hintze, Garry
Deliv	ery requ	ested by [Date] <u>03-28-08</u> Originator <u>Ga</u>	arry Christensen	
Dept.	Mgr/Sup	t. Date Station Manager Date	Operating Agent	Date

It should be noted that destruction of the burners occurred in less than two years since initial installation of the burners.

We feel that several failure mechanisms are occurring and not just one. We feel that they are:

1. Overheating of the tip in an out-of-service condition causing cracking in the tip due to tip design constraints. In the contract it was stated that "There are no environmental limitations to the coal burners. The reason for stating that there are no environmental limitations to the coal burners is that the stainless steel castings and plate facing the fire, ASTM 297 Gr He or 309 will not deteriorate at temperatures of at least 2,000 F. Consequently, ABT does not consider operation of its design in your boiler to have any environmental limitations. The conditions are such that no material will operate anywhere near its limit. In fact, ABT has placed no such limitation on any retrofit ABT has done.

Thermocouples were initially installed to monitor the tip and barrel temperatures. Out of service temperatures show that many burner tip temperatures did not even reach the 1600 F limit of the indications even though these burners experienced the same destruction. Cracking near the end of the tip do not appear to be connected to the cracking at the erosion areas.

- 2. Overheat and permanent deformation of the burner barrel causing excessive stress on the weld between the carbon steel barrel and tip casting. Barrel temperatures during an out-of service condition ranged from 700 to 1000 F. Typically each of the six burners on a row had different upper temperatures.
- 3. Material loss at the flower tip. The contractual proposal stated that "The segmented coal nozzle has an open design with no obstructions to wear or to collect coal and all wear is limited to the wear-resistant devices in the elbow." In less than two years, significant material loss at the flower tip ridges occurred. Cracking from these thinned areas has also occurred. Ductile materials can be very sensitive to abrasion-causing particles depending on the angle of impact. The angle of the tip ridges is around 18 degrees which is high on the erosion vs impact chart.

MEMORANDUM

INTERMOUNTAIN POWER SERVICE CORPORATION

TO:

George W. Cross

Page 1 of 1

FROM:

Dennis K. Killian

DATE:

September 13, 2007

SUBJECT:

Manual Requisition Approval for Failure Analysis on Burner Tip

Please approve the attached manual requisition for a failure analysis to be performed by Thielsch Engineering on an Advanced Burner Technology (ABT) burner tip.

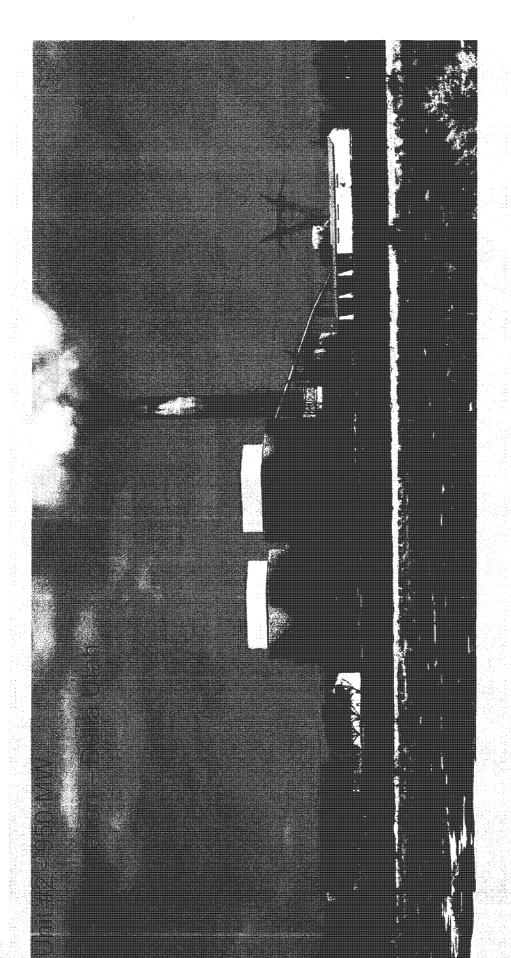
In the August 1, 2007 meeting at IPSC, Robert Allen from Siemens stated that from their analysis, the primary failure mechanism was erosion/thinning and then cracking propagated from the thinned areas. Technical Services personnel have also seen cracking not attached to any erosion areas and feel that an independent failure analysis on a failed ABT tip would be beneficial. This evaluation is not for contention purposes but to help verify and cover any other failure mechanisms so the new design will be successful.

The analysis work will be charged to work order 06-03474 Capital Project IGS07-2.

Any questions regarding this request may be directed to Garry Christensen at extension 6486.

GC/DEW:jmj Attachment

Intermountain Power Service Corp. ABT Siemens Warranty Claim



Date: October 17, 2007

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

ABT was awarded a contract in 2003 for the material supply of low NOx burners replacing existing B&W burners that had operated since 1992.

The base contract was for material supply only of 48 low NOx burners, 48 ABB Scanners plus air flow measuring equipment.

Approximately one year after commercial operation, the unit suffered a fire in one burner that destroyed the fuel injector. During the following Spring outage, Inspection revealed additional nozzles had cracks and excessive thinning of the fuel piping and nozzles.

April 2007, Siemens BTS and IPSC initiated a Six Sigma investigation to determine the root cause of the of the problems with the burners.

Siemens BTS and IPSC agreed on an issue statement with the five items:

- 1.) The alloy nozzle tip is cracking
- 2.) There is material loss at the following locations:

The burner nozzle tip

The "X" vane at the coal pipe elbow

The burner barrel

- 3.) The burner barrel is experiencing permanent deformation
- 4.) Establish the correct primary airflow for normal operation
- 5.) Definition of requirements for cooling air when the burner is out of service

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

The Six Sigma Root Cause analysis followed the five steps for a Six Sigma Project

Define: clear definition of the problem and the aim of the project

During the define stage, all available correspondence was collected, contract documents were collected, the involved parties were interviewed and an Issue Statement developed and agreed to.

Measure: Examination of the current process and collection relevant data for future analysis

The ABT design records were reviewed, the existing pulverizer performance at IPSC was documented and metallurgical analysis of the cracked burner nozzle was performed.

Analyze: Evaluation of the measured results and identification of the actual cause of the problem CFD analysis and thermal modeling of the nozzles using the operating parameters as measured during the pulverizer testing was performed. A root cause analysis was generated.

Improve: Selection and implementation of the solution

A new burner design was generated using the information collected during the Define and Measure stage and CFD analysis undertaken to verify changes will

Control: Control of the changed process

The differences between the original design and the revised design need to be implemented and documented

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

Executive Summary

The alloy nozzle tip cracking is the result of erosion of the wall thickness in the nozzle due to higher than original air and coal flow. The thinner wall section weakened the nozzle to the point that the nozzle could not accommodate the stress generated by the differential expansion between the stainless steel nozzle and the carbon steel barrel.

There is material loss at the burner nozzle tip, "X" vane at the coal pipe elbow and the burner barrel are a result of coal and air flows being higher than design plus stratification of the coal particles in the coal pipe entering the 90° elbow.

The burner barrel is experiencing permanent deformation due to higher than expected temperatures at the interface between the nozzle and barrel. The burner barrel will use a SS spool piece to extend back into the burner barrel.

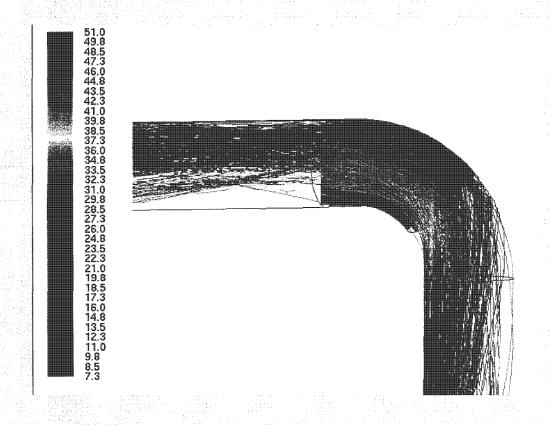
Establish the correct primary airflow for normal operation – The plant has not been operating per the B&W mill performance curve supplied in the contract. The mill curve supplied in the contract did not reflect the revision by B&W in 1992. Also, the plant has been operating at higher seal air flows

Definition of requirements for cooling air when the burner is out of service – the Operations and Maintenance manual will have to be revised to address out of service operation

Intermountain Power Service Corp ABT Siemens Warranty Claim

SIEMENS

Erosion and Mill Air Flow



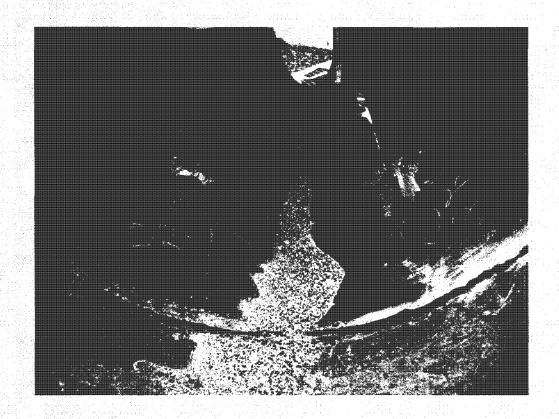
The CFD model shows the coal particles are stratified entering the elbow. The original kicker assembly with the X-vane that was modified to retain the clean out port will not last in the high velocity stream of concentrated coal particles with the higher coal flow.

The revised fuel injector design will increase the cross sectional area of the nozzle to reduce velocities, lengthen and flatten the slope of the transition ramp and replace the round elbow with a "Flat back" design to allow dispersion of the coal particles across the flow area of the nozzle.

Intermountain Power Service Corp ABT Siemens Warranty Claim

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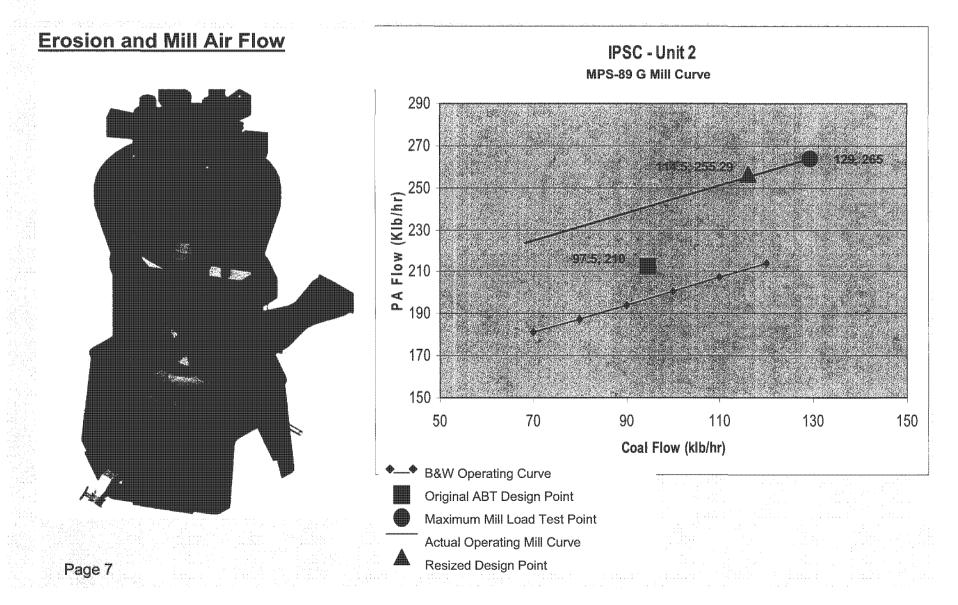
Erosion and Mill Air Flow



Erosion is originating at the transition slope from the round barrel to the 6 lobe exit. This is consistent with the results of the CFD model. The metallurgical analysis performed by Tordonato Energy Consultants identified erosion as a the contributor cause of the nozzle cracking. The high temperatures at the weld between the nozzle and burner barrel increased the stress which also contributed to the cracking. There was no evidence of corrosion.

Intermountain Power Service Corp ABT Siemens Warranty Claim

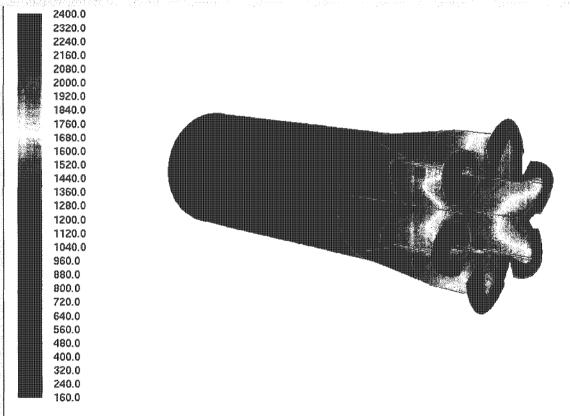
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Contours of Static Temperature (f)

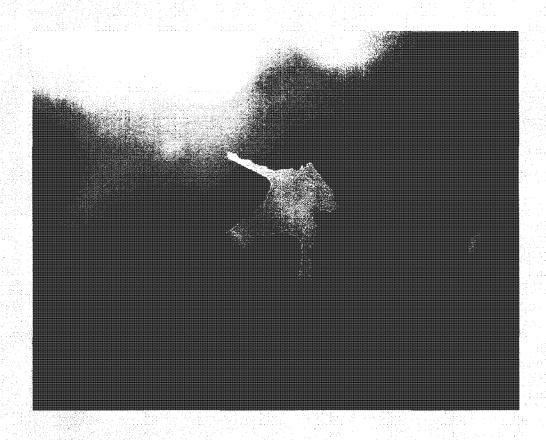
Sep 26, 2007 FLUENT 6.3 (3d, pbns, pdf20, rke)

The furnace radiation model shows that the heat conducted back to the burner barrel to be higher than expected. The revised fuel injector will use a spool piece of 253MA stainless steel to make the transition from the nozzle to the barrel. The revised fuel injector shall use refractory tile to shield the burner barrel from radiation from the furnace and to minimize erosion. This thermal model does not model the cooling of the secondary air on the tip.

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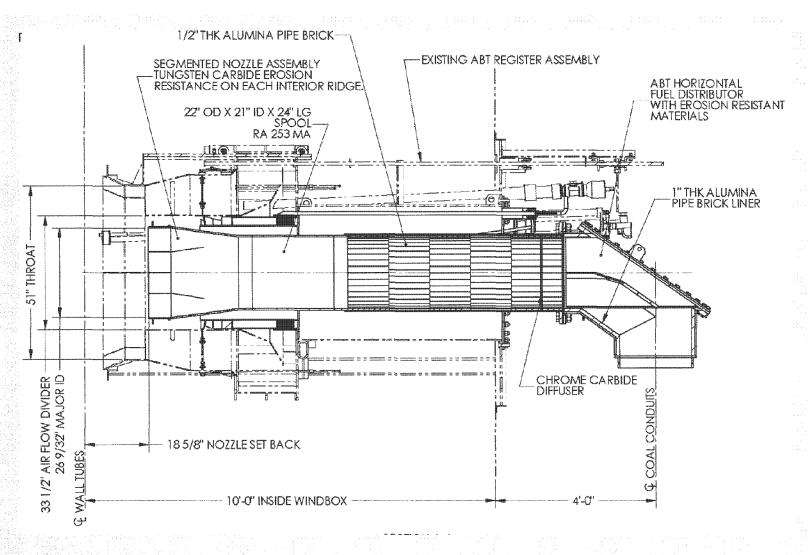
Thermal Stress



The off line burners are plugging with slag indicating that furnace gases are back flowing into the nozzle area. This creates very high temperatures that the nozzles were not designed for. A minimum air flow required to prevent this must maintained.

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Page 10

Intermountain Power Service Corp ABT Siemens Warranty Claim

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Next Steps

Close Out Six Sigma Program

•Commercial agreement between IPSC and Siemens Power Generation Inc

Agreement on Division of Responsibilities

Money to replace the burner injectors if needed is on the budget. Total replacement of the burners has not been pursued. One option that has been checked into is to replace the flowered ABT tips with straight tips from Power Industrial and make other repairs as needed. The lead time for the parts are 10-12 weeks. Power Industrial supplied Unit 1's nozzles and tips that have lasted over eight years. We have had very good success with their nozzle tip material. A 40" tip out of PI 2000 would be welded in to replace the flowered ABT tip as well as tips replaced last outage. This process was done on 15 burners in Spring 2006 but with nozzle tips removed from old nozzles and older B&W replacement nozzles. The coal nozzles could be modified to accommodate a conical diffuser and coal deflector similar to Unit 1 burner design. NOx would probably increase but we have OFA available on Unit 2.

Intermountain Generating Station
Unit 2 Burner Injector and Burner Elbow Replacement

Project Description

Replacement of all 48 burner elbows and burner injectors.

The existing burner injectors and burner elbows will be replaced with new injectors and sweep elbows provided by Siemens. The replaced injectors and elbows will be removed from the unit to a designated area. Burners are located on the 5th through the 8th level on the unit.

Scope of Work.:

- 1. Removal of old burner elbow on all 48 burners. (Just like 2006 outage)
 - a. Removal of welded TC from burner pipe.
 - b. Install needed rigging for burner pipe support.
 - c. Burner elbow removal by row.
 - d. Removal of old elbows to designated area outside of unit.
 - e. Clean flange mating surface.
- 2. Removal of old burner injector on all 48 burners. (Just like 2006 outage, 2000 # each)
 - a. Removal of lagging and insulation needed to unbolt injector.
 - i. Can happen at earlier sequence.
 - b. Unbolt injector and pull out of burner. Clean ash before pulling injector out.
 - c. Removal of old injectors to designated area outside of unit.
- 3. Clean up burner casing prior to installation of new injector.
 - a. Guzzle up all ash in burner casing and all ash that has fallen into burner secondary air opening.
 - b. Repair burner casings as needed. ** Inspection 2 years ago showed damage on several burner casings per row. We will not know the extent of repairs needed until injector pulled.
- 4. Installation of 48 new burner injectors.
 - a. Unload upon arrival and mobilize new burner injectors to appropriate burner rows.
 - b. Install new burner injectors by sliding into burner casing and bolting up to burner housing with gasket material.
 - c. Install insulation and lagging. (Can be installed after elbow installation)
- 5. Installation of 48 new flat back burner elbows.
 - a. Unload upon arrival and mobilize new burner flat back elbows to appropriate burner rows.
 - b. Position and bolt up 48 new burner elbows with gasket material.

- 6. General cleanup following completion of installation.
- 7. Painting
 - a. After completion of installation (April 21, 2008 at 07:00) IPSC painters to prep elbows and paint. Stencil elbows for identification. i.e. C-1, C-2,....
- 8. Schedule:
 - a. Injectors and flat back elbows:
 - i. Start of work: March 28, 2008 or as soon as required materials are on site.
 - ii. <u>Completion</u>: Installation and inspections of burner injector and elbows by April 21, 2008 at 07:00
- 9. Materials:
 - a. Materials to be supplied by Siemens.
 - i. Burner fuel injector.
 - ii. Flat back elbows with x-vane.
 - b. Material s supplied by IPSC.
 - i. Gasket material for burner elbow flanges.
 - ii. Gasket material for injector to burner housing.
 - iii. 253 MA material to repair burner casings.
 - c. The contractor shall be responsible for providing weld rod, all additional parts, tools, and/or materials including insulation and lagging required for the completion of this job.